

## Block Copolymer at Nano-Patterned Surfaces

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**ABSTRACT:** We present numerical calculations of lamellar phases of block copolymers at patterned surfaces. We model symmetric diblock copolymer films forming lamellar phases and the effect of geometrical and chemical surface patterning on the alignment and orientation of lamellar phases. The calculations are done within self-consistent field theory (SCFT), where the semi-implicit relaxation scheme is used to solve the diffusion equation. Two specific setups, motivated by recent experiments, are investigated. In the first, the film is placed on top of a surface imprinted with long chemical stripes. The stripes interact more favorably with one of the two blocks and induce a perpendicular orientation in a large range of system parameters. However, the system is found to be sensitive to its initial conditions and sometimes gets trapped into a metastable mixed state composed of domains in parallel and perpendicular orientations. In a second setup, we study the film structure and orientation when it is pressed against a hard grooved mold. The mold surface prefers one of the two components, and this setup is found to be superior for inducing a perfect perpendicular lamellar orientation for a wide range of system parameters.

### I. Introduction

Block copolymers (BCPs) have been studied extensively in the last few decades because of their special self-assembly properties giving rise to interesting mesophases in the submicrometer-to-nanometer range as well as to their numerous applications, where desired properties can be tailored by specific chain architecture.<sup>1–8</sup>

Bulk properties of BCPs are rather well understood and, in recent years, much effort was devoted to understand thin films of BCP. One potential application is the use of thin films of diblock copolymers as templates and scaffolds for the fabrication of arrays of nanoscale domains, with high control over their long-range ordering and with the hope that this technique can be useful in future micro- and nanoelectronic applications. Recent experiments include using chemically<sup>9–18</sup> and physically<sup>19–22</sup> patterned surfaces, which have preferential local wetting properties for one of the two polymer blocks. The orientation and alignment of lamellar and hexagonal phases of BCP and, in particular, their transition between parallel and perpendicular orientations were investigated. Another useful method is the use of electric fields to orient anisotropic phases of BCP, such as lamellar and hexagonal, in a direction perpendicular to the solid surface.<sup>23–31</sup>

In this article, we present self-consistent field theory (SCFT) calculations inspired by recent experiments on patterned surfaces.<sup>10–14,32–34</sup> Our main aim is to analyze what are the thermodynamical conditions that facilitate the perpendicular orientation of BCP lamellae with respect to the underlying solid surface, and how the lamellar ordering can be optimized. Two specific solid patterns and templates are modeled. The first is a planar solid surface that has a periodic arrangement of long and parallel stripes preferring one of the two blocks but otherwise is neutral to the two blocks in its interstripe regions. We show that this experimentally realized surface pattern<sup>10–14</sup> enhances the perpendicular lamellar orientation. The second surface pattern is motivated by recent NanoImprint lithography (NIL) experiments.<sup>14,32–34</sup> This

is a high-throughput low-cost process that has the potential of reducing the need for costly surface preparation. Here a hard grooved mold is pressed onto a thin BCP film at temperatures above the film glass transition and induces perpendicularly oriented lamellae. Within our model, we show that indeed the grooved surface does enhance the perpendicular orientation of lamellae.

The SCFT model has several known limitations. It is a coarse-grained model and, as such, can only describe spatial variations that are equal or larger than the monomer size (the Kuhn length). Our calculations provide the thermodynamical equilibrium or local minima of the film free-energy in the presence of geometrical constraints. Therefore, important structural details induced by hydrodynamic flow and film rheology as occurring during sample preparation are not described by the model.

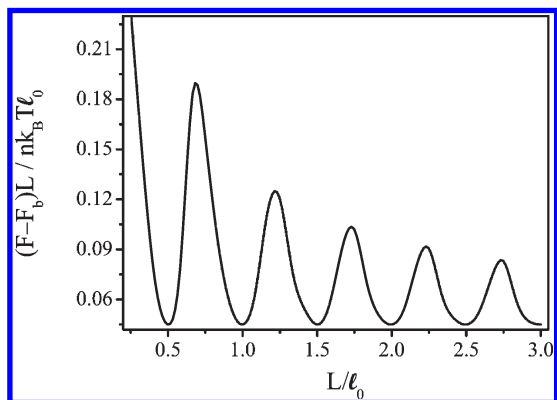
In the present work, we limit ourselves to 3D systems that are translationally invariant along one spatial direction. This is applicable when the BCP film is put in contact with surfaces having long unidirectional stripes or grooves. Extensions of the present work to more complex 3D systems with 2D surface patterns will be addressed separately in a follow-up publication.

The outline of our article is as follows. In the next section, two system setups are introduced; a chemically striped surface and a grooved mold and their effect on orienting lamellar BCP films are presented. In Section III, we describe our SCFT model and how its equations are solved numerically. In Section IV, our results are presented for the two types of experimental setups. Finally, in the last section, we discuss the model predictions and their connection with experimental findings.

### II. BCP Film Design

We consider a melt of A–B diblock copolymer (BCP) chains composed of  $n$  chains, each having a length  $N = N_A + N_B$  in terms of the Kuhn length,  $a$ , which is assumed, for simplicity, to be the same for the A and B monomers. Therefore, the A-monomer molar fraction  $f = N_A/N$  is equal to its volume fraction. In addition, hereafter we concentrate on symmetric di-BCP,  $N_A = N_B$ , having

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**Figure 1.** Difference of the dimensionless film free energy from its bulk value,  $(F - F_b)L / (nk_B T l_0)$ , as function of the film rescaled thickness,  $L/l_0$ , where  $l_0$  is the lamellar periodicity,  $k_B T$  is the thermal energy, and  $n$  is the total number of chains. The lamellae in the film are parallel to the two flat bounding surfaces (the  $L_{\parallel}$  state). The surface preference is  $\Delta u = 1$  for the bottom surface and  $\Delta u = 0$  for the top, and  $N\chi = 20$ .

$f = 0.5$ . The symmetric BCP yields thermodynamically stable lamellar phases of periodicity  $l_0$  as the temperature is lowered below the order–disorder temperature (ODT).<sup>35</sup> At shallow temperature quenches, simple scaling arguments<sup>36</sup> used in the weak segregation limit show that the lamellar period  $l_0$  is proportional to  $R_g$ , the chain radius of gyration,  $l_0 \sim R_g = (Na^2/6)^{1/2} \sim N^{1/2}$ . For deep temperature quenches well below the ODT, the strong segregation theory<sup>37</sup> yields more stretched chains as  $l_0 \approx N^{2/3} \gg R_g \sim N^{1/2}$ .

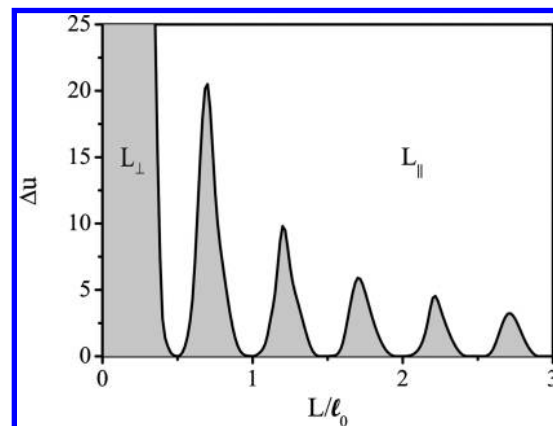
The BCP film has total volume  $\Omega$  and lateral area  $A$ , so that its thickness is  $L = \Omega/A$ . In some experimental setups, the BCP film is bounded by two planar solid surfaces, and its thickness,  $L$ , is a constant. In other setups,<sup>10–14</sup> the film is spin coated on a solid surface with a free polymer/air interface on its top so that the thickness can vary spatially. In yet another setup used in NIL experiments,<sup>14,32–34</sup> a grooved mold is pressed against the film, and the film penetrates into the mold. Because the film profiles inside the mold vary considerably in height,  $L$  is only the film average thickness.

We will consider only surface features along one spatial direction (chosen to be the  $x$  direction) and assume that the system is translationally invariant along the second surface direction (the  $y$  direction). Therefore, the film volume  $\Omega$  (per unit length) has units of length square, whereas the surface area,  $A$ , has units of length. The third spatial direction, the  $z$  directions, is taken to be perpendicular to the surfaces. This allows us to carry out the numerical calculations only in the  $(x, z)$  2D plane and represents a considerable simplification from the numerical point of view.

The situation where a thin BCP film is placed in contact with a flat and uniform surface (or is sandwiched between two flat surfaces) was modeled by several authors.<sup>36,38–46</sup> Two main features are apparent when the film behavior is compared with that of bulk BCP. The first effect is the film confinement. When  $L$  differs from multiples of half the natural periodicity  $l_0$ , the chains need to be stretched or compressed because the film is incompressible and space-filling. The film free-energy shown in Figure 1 is a function of the thickness,  $L$ , is obtained within our SCFT scheme (see below), and agrees well with previous results.<sup>38,43</sup>

The main effect of the confinement between the two bounding surfaces is the existence of free-energy minima at integer or half-integer values of  $L/l_0 = 1/2, 1, 3/2, \dots$  corresponding to film thicknesses where we can fill an integer or half-integer numbers of A–B parallel layers in between the two surfaces. The overall trend for the film free energy is to converge toward the bulk value  $F_b$  as:  $F - F_b \sim 1/L$ .

The second feature is the possibility of inducing a parallel-to-perpendicular transition of the lamellae by changing the strength



**Figure 2.** Phase diagram for intermediately segregated ( $N\chi = 20$ ) symmetric diblock lamellar phase in terms of the film thickness  $L/l_0$  versus the surface field preference between the two blocks,  $\Delta u = u_A - u_B$  (in units of  $Nk_B T$ ). The gray area indicates the perpendicular lamellar region ( $L_{\perp}$ ), and the white region above it is the parallel state ( $L_{\parallel}$ ). The film is confined in the  $z$  direction between two parallel and flat surfaces. The bottom surface uniformly attracts one of blocks ( $\Delta u > 0$ ), whereas the top one mimics the free (and neutral) surface,  $\Delta u = 0$ .

of the surface preference,  $\Delta u$ . This can be seen in Figure 2, where the parallel to perpendicular phase diagram is plotted in the  $\Delta u$ – $L$  plane, within our SCFT scheme. When a strong surface preference toward one of the two blocks is included, the lamellae tend to orient in a parallel direction, whereas for neutral (indifferent) surfaces or weak preferences, the perpendicular orientation is preferred because the lamellae can assume their natural periodicity  $l_0$  in this orientation for any thickness,  $L$ . Note also that the transition occurs at  $\Delta u = 0$  for integers or half-integers values:  $L/l_0 = 1/2, 1, 3/2, \dots$ , as was argued above. These results agree well with those reported in refs 36, 38, and 43.

In the remainder of the article, we will address in detail the question of how it is possible to better control the relative stability of parallel and perpendicular phases of lamellar BCP films and, in particular, how the stability of the perpendicular phase can be increased for a larger range of film thicknesses and surface characteristics.

### III. Theoretical Framework

Because the system is translationally invariant in the  $y$  direction, we treat it as an effective 2D system. The free energy for such a diblock copolymer (BCP) film confined between the two surfaces is

$$\begin{aligned} \frac{a^2}{k_B T} F = & \int d^2 r [\chi \phi_A(r) \phi_B(r) - \omega_A(r) \phi_A(r) - \omega_B(r) \phi_B(r)] \\ & - na^2 \ln Q_C - \int d^2 r [u_A(r) \phi_A(r) + u_B(r) \phi_B(r)] \\ & + \int d^2 r \eta(r) [\phi_A(r) + \phi_B(r) - 1] \end{aligned} \quad (1)$$

where each of the  $n$  BCP chains is composed of  $N = N_A + N_B$  Kuhn segments of length  $a$ , and the Flory–Huggins parameter is  $\chi$ . The dimensionless volume fractions of the two components are defined as  $\phi_A(r) = \phi_A(x, z)$  and  $\phi_B(r) = \phi_B(x, z)$ , respectively, whereas  $\omega_j(r)$ ,  $j = A, B$  are the auxiliary fields coupled to  $\phi_j(r)$ , and  $Q_C$  is the single-chain partition function in the presence of the  $\omega_A$  and  $\omega_B$  fields. (See eqs 4 and 5 below for more details.) The third term represents a surface energy preference, where  $u_A$  and  $u_B$  are the short-range interaction parameters of the surface with the A and B monomers, respectively. Formally,  $u_A(r)$  and  $u_B(r)$  are surface fields and get nonzero values only on the surface(s).

Finally, the last term includes a Lagrange multiplier  $\eta(r)$  introduced to ensure the incompressibility condition of the BCP melt

$$\phi_A(r) + \phi_B(r) = 1 \quad \text{for all } r \in \Omega \quad (2)$$

By inserting this condition, eq 2, in the surface free energy of eq 1, the integrand becomes  $u_A\phi_A + u_B\phi_B = (u_A - u_B)\phi_A + u_B$ . Therefore,  $\Delta u(r) \equiv u_A(r) - u_B(r)$  is the only needed surface preference field that will be employed throughout the article.

Using the saddle-point approximation, we obtain a set of self-consistent equations

$$\begin{aligned} \frac{\delta F}{\delta \phi_A} = 0 &\Rightarrow \omega_A(r) = \chi\phi_B(r) - u_A(r) + \eta(r) \\ \frac{\delta F}{\delta \phi_B} = 0 &\Rightarrow \omega_B(r) = \chi\phi_A(r) - u_B(r) + \eta(r) \\ \frac{\delta F}{\delta \omega_A} = 0 &\Rightarrow \phi_A(r) = \frac{na^2}{\Omega Q_C} \int_0^{N_A} ds q_A(r, s) q_A^\dagger(r, N_A - s) \\ \frac{\delta F}{\delta \omega_B} = 0 &\Rightarrow \phi_B(r) = \frac{na^2}{\Omega Q_C} \int_0^{N_B} ds q_B(r, s) q_B^\dagger(r, N_B - s) \end{aligned} \quad (3)$$

where the incompressibility condition, eq 2, is obeyed, and the single-chain free energy,  $Q_C$ , is

$$Q_C = \frac{1}{\Omega} \int d^2r q_A^\dagger(r, N_A) \quad (4)$$

The two types of propagators  $q_j(r, s)$  and  $q_j^\dagger(r, s)$  (with  $j = A, B$ ) are solutions of the modified diffusion equation

$$\frac{\partial q_j(r, s)}{\partial s} = \frac{a^2}{6} \nabla^2 q_j(r, s) - \omega_j(r) q_j(r, s) \quad (5)$$

with the initial condition  $q_A(r, s=0) = q_B(r, s=0) = 1$ ,  $q_A^\dagger(r, s=0) = q_B^\dagger(r, N_B)$ , and  $q_B^\dagger(r, s=0) = q_A^\dagger(r, N_A)$ , where  $s$  is a conveniently defined curvilinear coordinate along the chain contour. This diffusion equation is solved using reflecting boundary conditions at the two confining surfaces ( $z=0$  and  $z=L$ ):  $dq/dr|_{z=0} = 0$  and  $dq/dr|_{z=L} = 0$ , whereas periodic boundary conditions are used in the perpendicular direction.

Hereafter, we rescale all lengths by the natural periodicity of the BCP,  $l_0 \approx 4.05R_g$ ,<sup>47</sup> where  $R_g$  is the chain radius of gyration  $R_g^2 = Na^2/6$ . Similarly,  $s$  is rescaled by  $N$ , yielding  $r \rightarrow r/l_0$ ,  $s \rightarrow s/N$ ,  $\chi \rightarrow N\chi$ ,  $\omega_j(r) \rightarrow N\omega_j(r)$ , and  $u_j(r) \rightarrow Nu_j(r)$  with  $j = A$  or  $B$ . With this rescaling, we rewrite the self-consistent equations as

$$\omega_A(r) = \chi\phi_B(r) - u_A(r) + \eta(r) \quad (6)$$

$$\omega_B(r) = \chi\phi_A(r) - u_B(r) + \eta(r) \quad (7)$$

$$\phi_A(r) = \frac{1}{Q_C} \int_0^f ds q_A(r, s) q_A^\dagger(r, f - s) \quad (8)$$

$$\phi_B(r) = \frac{1}{Q_C} \int_0^{1-f} ds q_B(r, s) q_B^\dagger(r, 1 - f - s) \quad (9)$$

$$\frac{\partial q_j(r, s)}{\partial s} = \left(\frac{R_g}{l_0}\right)^2 \nabla^2 q_j(r, s) - \omega_j(r) q_j(r, s) \quad (10)$$

where  $f = N_A/N$ ,  $\Omega_1 \equiv \Omega/l_0^2$ , and  $Q_C = (1/\Omega_1) \int d^2r q_A^\dagger(r, f)$ . Note that the incompressibility condition, eq 2, together with eqs 6 and 7 can be used to obtain the Lagrange multiplier  $\eta(r)$

$$\eta(r) = \frac{1}{2} (\omega_A + \omega_B - \chi + u_A + u_B) \quad (11)$$

With the rescaled variables, we define now a rescaled free energy

$$\begin{aligned} \frac{Na^2}{\Omega_1 l_0^2} \frac{F}{k_B T} = \frac{F}{nk_B T} = \frac{1}{\Omega_1} \int d^2r [\chi\phi_A(r)\phi_B(r) - \omega_A(r)\phi_A(r) \\ - \omega_B(r)\phi_B(r)] - \ln Q_C - \frac{1}{\Omega_1} \int d^2r [u_A(r)\phi_A(r) + u_B(r)\phi_B(r)] \\ + \frac{1}{\Omega_1} \int d^2r \eta(r) [\phi_A(r) + \phi_B(r) - 1] \end{aligned} \quad (12)$$

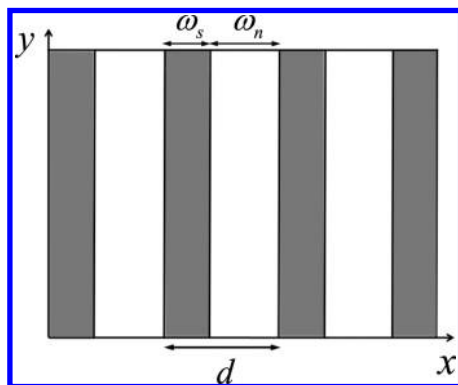
The above self-consistent equations can be solved numerically in the following way. First, we guess an initial set of values for the auxiliary fields  $\omega_j(r)$ . Then, through the diffusion equations, eq 10, we calculate the propagators,  $q_j$  and  $q_j^\dagger$ . Next, we calculate the monomer volume fractions  $\phi_j$  from eqs 8 and 9 and the Lagrange multiplier  $\eta(r)$  from eq 10. We can now proceed with a new set of values for  $\omega_j(r)$  obtained through eqs 6 and 7, and this procedure can be iterated until convergence is obtained by some conventional criterion described below.

We use the semi-implicit relaxation scheme<sup>48</sup> to solve the 2D modified diffusion equations, eq 10. Our convergence criterion is based on the incompressibility condition. For perfect structures such as parallel or perpendicular lamellae, the maximum allowed deviation between the sum of the A and B densities and unity,  $|1 - \phi_A(r) - \phi_B(r)|$ , is  $10^{-4}$ , whereas for the mixed  $L_M$  phase (see below), it is around  $10^{-2}$ . As mentioned above, we rescale all lengths by the natural periodicity of the BCP,  $l_0 \approx 4.05R_g$ , and the curvilinear coordinate,  $s$ , by the total number of monomers in one chain,  $N$ . The spatial discretization in the  $x$  direction is 0.05 (in units of  $l_0$ ), whereas in the  $z$  direction, it is 0.025. The discretization of the  $s$  variable is 0.02. For all presented results, the free energy changes in the last few iteration steps are  $< 10^{-4}$  in units of  $k_B T/\text{chain}$  after the first 1000 iterations and decrease to  $10^{-6}$  after an additional 4000 iterations. Note that because we work at a mean-field level (SCFT), it would not be of advantage to refine the convergence of the free energies to a higher accuracy further because we neglect any quadratic fluctuations that might give larger corrections.

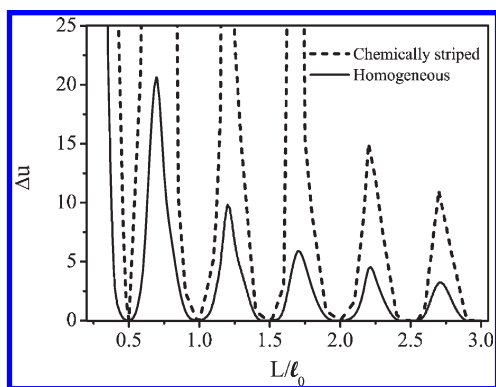
#### IV. Results

We present now the numerical results for symmetric diblock films ( $f = 1/2$ ) at various patterned surfaces. The natural periodicity of the BCP,  $l_0$ , is chosen for all numerical calculations to be 50 nm. This value roughly corresponds to values used in several experimental setups.<sup>12-14</sup> All lengths are rescaled by  $l_0$ , as was explained in Section III. Except when explicitly mentioned, all results are obtained by using the fully disordered phase of the BCP film,  $\phi_A(r) = \phi_B(r) = 0.5$ , as initial condition. Then, a temperature quench is performed from the disordered state above the ODT to temperatures below the ODT where the lamellar phase is stable.

**A. Chemically Striped Surface.** The system is modeled using a SCFT scheme for two separate setups that are motivated by recent experiments.<sup>10-14</sup> In the first setup, the BCP film is spread on a flat but chemically patterned solid surface, whereas the second bounding surface is the free film/air interface, which is either neutral or has a slight preference toward one of the two BCP components. In our calculations, we take this top surface to be always neutral. A top view of the bottom patterned surface can be seen in Figure 3 and is composed of infinitely long stripes in the  $y$  direction of width  $\omega_s \approx 100$  nm that prefer the A component ( $\delta u > 0$ ). These stripes are separated by neutral interstripe regions of width  $\omega_n$  having the same affinity for A and B ( $\Delta u = 0$ ). Because the stripes are infinitely long in the  $y$  direction, the chemical surface pattern has a 1D



**Figure 3.** Top view of a striped surface lying in the  $x$ - $y$  plane. The periodicity is  $d = \omega_s + \omega_n$ , where the A-preferring stripes have a width of  $\omega_s$  and the neutral interstripe regions are of width  $\omega_n$ .



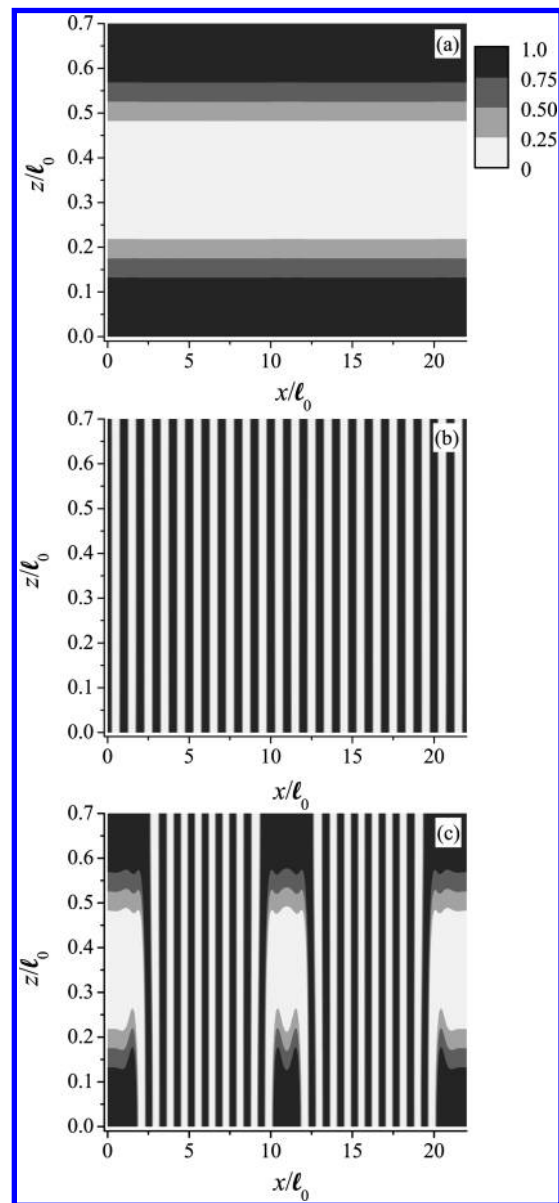
**Figure 4.** Phase diagram in terms of the film thickness  $L$  versus the surface preference  $\Delta u$  for chemically striped surface (dashed line) and homogeneous surface (solid line). The lines separate the parallel phase ( $L_{||}$ ) for larger  $\Delta u$  values from perpendicular one ( $L_{\perp}$ ) at smaller  $\Delta u$  values. The parameters used are  $N\chi = 20$  and  $l_0 = 50$  nm, and for the striped surface,  $\omega_s = 2l_0$  and  $\omega_n = 8l_0$  so that  $d = 10l_0 = 500$  nm.

square-wave shape and is periodic in the  $x$  direction,  $\Delta u(x+d) = \Delta u(x)$ , with periodicity  $d = \omega_s + \omega_n$

$$\begin{aligned} \Delta u(x) &= u_s \quad \text{for } 0 < x \leq \omega_s \\ \Delta u(x) &= u_n \quad \text{for } \omega_s < x \leq d \end{aligned} \quad (13)$$

Note that we can write formally the surface preference field  $\Delta u = u_A - u_B$  as  $\Delta u(r) = \Delta u(x)\delta(z)$ , where  $\delta(z)$  is the Dirac delta function. All numerical values of  $\Delta u$  are given hereafter in terms of its rescaled units,  $\Delta u \rightarrow N\Delta u$ .

In the following, we fix the width  $\omega_s$  to be twice the natural periodicity, yielding  $\omega_s = 2l_0 = 100$  nm. The phase diagram shown in Figure 4 is calculated in terms of the film thickness,  $L$ , and the bottom surface preference,  $\Delta u$ , for this setup and compared with the one in Figure 2 for homogeneous surfaces. All parameters here are taken to be the same as that for the homogeneous surface, except that the bottom surface has chemical stripes. Furthermore, we fix the value of the inter-stripe distance (where there is no preferred adsorption), to  $\omega_n = 8l_0 = 400$  nm so that the pattern periodicity is  $d = \omega_s + \omega_n = 500$  nm, or  $10l_0$ . The phase diagram is obtained by starting as an initial guess from the perpendicular lamellar phase ( $L_{\perp}$ ) or the parallel one ( $L_{||}$ ). After convergence, their free energies are compared. From the Figure, it is evident that the  $L_{\perp}$  phase has a larger stability range for the chemically striped surface as compared with the homogeneous surface, although the effective value of  $\Delta u$  on the entire patterned surface is smaller because its value should be averaged over both the striped and interstripe regions:  $\Delta u_{\text{eff}} = \Delta u(\omega_s/d)$ .



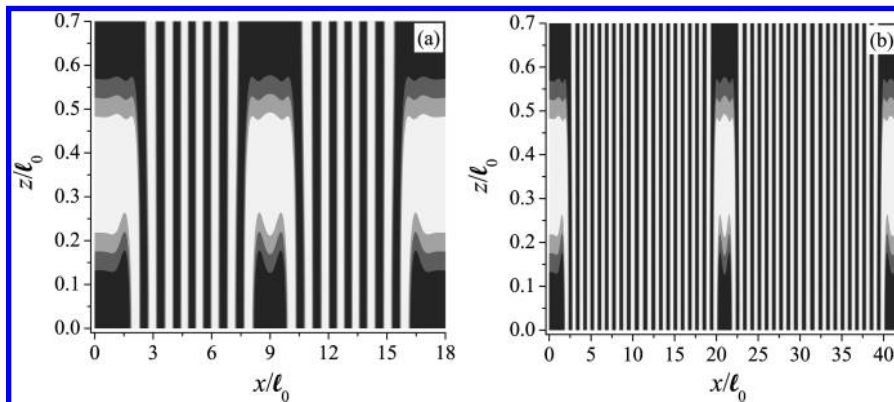
**Figure 5.** BCP lamellar structures obtained from numerical solutions of SCFT equations for three different initial conditions: (a) parallel lamellar ( $L_{||}$ ), (b) perpendicular lamellar ( $L_{\perp}$ ), and (c) fully disordered state developing into a mixed morphology ( $L_M$ ) in registry with the striped surface. The film thickness is  $L = 0.7l_0$ , and the top surface is taken as neutral,  $\Delta u = 0$ , whereas the bottom one has a striped pattern, as in Figure 3 with  $\Delta u = 1$ . The stripe widths are set to be  $\omega_s = 2l_0$  and  $\omega_n = 8l_0$ , yielding  $d = \omega_s + \omega_n = 10l_0 = 500$  nm. The other parameters are  $N\chi = 20$  and  $l_0 = 50$  nm. The color code corresponds to the four intervals of local monomer density  $0 \leq \phi_A(r) \leq 1$ , as is depicted in part a.

Note that the stability of the  $L_{\perp}$  phase is particularly enhanced for special values of  $L$ :  $L/l_0 = 3/4, 5/4$ , and so on.

Because of the existence of many metastable states in BCP melts, the numerical procedure of free energy minimization is sensitive to the initial conditions. Instead of always converging to the true equilibrium structure at any point of the phase diagram, different metastable structures can be obtained. We show some results to illustrate this scenario in Figure 5.

For  $L = 0.7l_0$ ,  $d = 10l_0$ ,  $\Delta u = 1$ , and  $N\chi = 20$  (a typical set of parameters that is located inside the  $L_{\perp}$  stable region), we start with parallel lamellae, perpendicular lamellae, and the fully disordered state as three different initial conditions and perform a temperature quench to a temperature below the ODT. The  $L_{||}$  and  $L_{\perp}$  phases in Figure 5a,b, respectively, result





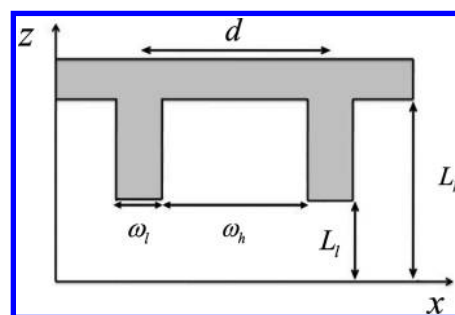
**Figure 6.** Calculated BCP lamellar structures for patterned surfaces of increasing interstripe distance  $\omega_n$  while  $\omega_s = 2l_0$  remains fixed (and, hence, increasing  $d$ ). (a)  $\omega_n = 6l_0$  and  $d = 8l_0 = 400$  nm. (b)  $\omega_n = 18l_0$  and  $d = 20l_0 = 1$   $\mu$ m. All lengths are scaled with the lamellar periodicity  $l_0 = 50$  nm. The other parameters are:  $L = 0.7l_0$ ,  $\Delta u = 1$ , and  $N\chi = 20$ . The initial condition is chosen as the fully disordered state,  $\phi_A(r) = 0.5$ , and all other parameters and color code are the same as those in Figure 5. The system exhibits mixed  $L_M$  morphologies with  $L_{\perp}$  regions just on top of the surface stripes and perfect  $L_{\perp}$  domains in between the stripes.

from quenching from  $L_{\parallel}$  and  $L_{\perp}$  initial conditions. Therefore, the system retains its orientation after the temperature quench. For the fully disordered initial condition, we obtain a mixed structure containing domains of the  $L_{\parallel}$  and  $L_{\perp}$  phases in registry with the striped surface. This structure is shown in Figure 5c and is coined as  $L_M$ .

As explained in Section III, the maximal deviation of the incompressibility condition,  $|1 - \phi_A(i, j) - \phi_B(i, j)|$ , serves as our accuracy criterion. It is  $1.10 \times 10^{-6}$  for the parallel lamellae as initial condition (Figure 5a);  $2.57 \times 10^{-5}$  for the perpendicular lamellae as initial condition (Figure 5b); and  $1.07 \times 10^{-2}$  for disordered state as initial condition (Figure 5c). For  $L_{\parallel}$  and  $L_{\perp}$ , it is quite small, yielding a value of about  $10^{-5}$ . However, it is not as good in the mixed  $L_M$  structure ( $\sim 10^{-2}$ ) because of the existence of internal boundaries between parallel and perpendicular domains. To answer the question of metastability, we calculate the free energies per chain and obtain  $f_{\parallel} = 4.272 > f_M = 4.122 > f_{\perp} = 4.061$  corresponding to the  $L_{\parallel}$ ,  $L_M$  and  $L_{\perp}$  phases, respectively. Clearly, the most stable structure is the perpendicular one,  $L_{\perp}$ , and is consistent with our phase diagram in Figure 4. Note that the free-energy differences between the various states are very small, on the order of 2–5%, manifesting the tendency of the system to get trapped into metastable states.

Our findings also have experimental implications because in experiments, the film structure depends strongly on its history and sample preparation.<sup>14,33,34</sup> The claim is that once the system is prepared in its  $L_{\perp}$ , it will stay there, but if the film is prepared above the ODT, in its fully disordered state, then the film can get stuck in a metastable mixed lamellar structure,  $L_M$ . Although in experiments, it is not always possible to heat the system above its ODT because of polymer breakdown and oxidation, in many cases, higher temperatures are used to anneal the film and allow it to reach its final state via faster dynamics.

Another interesting feature is presented in Figure 5c. Perfect perpendicular lamellar structures between neighboring stripes are visible. Furthermore, we can obtain such perfect  $L_{\perp}$  structures for a wide range of small and large periodicities, ranging from  $d = 400$  nm in Figure 6a to  $d = 1$   $\mu$ m =  $20l_0$  in Figure 6b. However, we find that it is difficult to get rid of the parallel lamellar regions induced by the striped pattern, even when we further reduce the BCP film thickness  $L$  to values much less than  $l_0$  and decrease the values of  $\Delta u$ . Furthermore, a preliminary study<sup>49</sup> indicates that slow temperature annealing from the disorder state (above ODT) to the ordered lamellar state (below ODT) does not seem to prevent the formation of the mixed  $L_M$  phase.



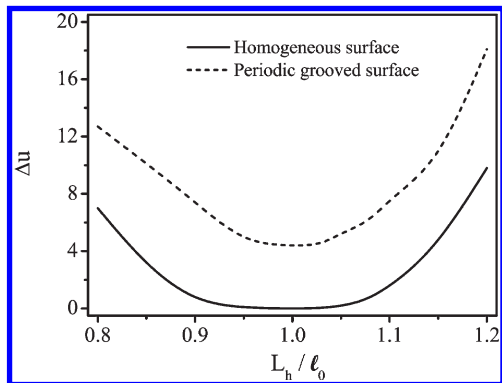
**Figure 7.** Cut (side view) through the top grooved surface (the mold) used in NIL. The periodicity in the  $x$  direction is  $d = \omega_1 + \omega_n$ , with  $\omega_1$  and  $\omega_n$  being the finger and interfinger width, respectively.  $L_1$  is the distance of closest approach to the bottom surface at  $z = 0$ , and  $L_h$  is the largest film thickness. The initial film thickness is equal to the average film thickness in the mold,  $L = (L_1\omega_1 + L_h\omega_n)/d$ .

**B. Periodic Grooved Surfaces.** To overcome the problem of getting trapped in  $L_M$  mixed states and inspired by recent NanoImprint lithography (NIL) experiments,<sup>14,32–34</sup> we explored yet another type of surfaces. The setup can be seen in Figure 7, where the BCP film is confined between two solid surfaces. The bottom surface at  $z = 0$  is flat, whereas the top one has a periodic arrangement of grooves (along the  $x$  direction) made of a series of down-pointing “fingers” of thickness  $\omega_1$ , separated by intergrooves regions (“plateaus”) of thickness  $\omega_n$ . The periodic height profile  $h(x) = h(x + d)$  has the form

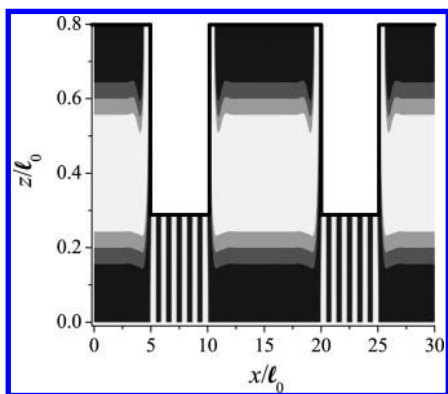
$$\begin{aligned} h(x) &= L_1 \quad \text{for } 0 < x \leq \omega_1 \\ h(x) &= L_h \quad \text{for } \omega_1 < x \leq d \end{aligned} \quad (14)$$

where the height is measured from the  $z = 0$  surface. Formally,  $\Delta u(r) = u_A - u_B$  used in the solution of eqs 6 and 7 is given by  $\Delta u(r) = \Delta u(x)\delta(z - h(x))$ .

The Figure shows the surface height profile in the  $x$ - $z$  plane for profiles that are translationally invariant in the  $y$  direction. The periodicity in the  $x$  direction is  $d = \omega_1 + \omega_n$ , and the finger width is chosen to be  $\omega_1 = 5l_0 = 250$  nm. The top surface (mold) is put in direct contact with a BCP film spread on a neutral and flat bottom surface (at  $z = 0$ ). The distance of closest approach between the two surfaces is  $L_1$ , whereas the maximal height difference between them is  $L_h$ . This means that the finger height of the mold is  $L_h - L_1$ . Assuming film incompressibility, we get a relation between the thickness  $L$  of the original BCP film and the two height



**Figure 8.** Phase diagram (as in Figure 4) in terms of the maximal film thickness  $L_h$  versus the surface field difference of the two blocks,  $\Delta u$ , for a periodic grooved surface (dashed line) and a homogeneous surface (solid line). The lines separate between the  $L_{||}$  and  $L_{\perp}$  phases. In the latter case, the film thickness  $L$  is equated with  $L_h$ . Other parameters are:  $l_0 = 50$  nm,  $L_1 = 0.3l_0$ ,  $d = 15l_0 = 750$  nm,  $\omega_1 = 5l_0 = 250$  nm,  $\omega_h = 10l_0 = 500$  nm, and  $N\chi = 20$ .



**Figure 9.** BCP density distribution for an  $L_M$  phase for  $d = 15l_0 = 750$  nm and  $N\chi = 20$  starting from a fully disordered initial condition. The bottom surface is neutral, and the top surface has a square wave height profile as in Figure 7, where  $\Delta u = 0.1$ . Other parameters are  $L_h = 0.8l_0$  and  $L_1 = 0.3l_0$ ,  $\omega_h = 10l_0$  and  $\omega_1 = 5l_0$ , yielding  $L/l_0 = 1.9/3 \approx 0.64$ .

parameters,  $L_1$  and  $L_h$ :  $L = (L_1\omega_1 + L_h\omega_h)/d$ . In experiments, the average thickness  $L$  is fixed, whereas in the numerical study, we directly control  $L_1$  and  $L_h$ .

By varying the values of the parameters  $d$ ,  $L_h$ , and  $L_1$  of the mold and the strength of surface interactions  $\Delta u$ , we can get a sequence of BCP patterns. Furthermore, we obtain perfect perpendicular lamellar structures extending throughout the film thickness for some special patterned surfaces.

We calculate the phase diagram in terms of the maximal film thickness,  $L_h$ , versus the surface preference,  $\Delta u = u_A - u_B$ . The interaction strength on all exposed surfaces of the upper grooved mold has the same value of  $\Delta u$ . In addition, we set  $L_1 = 0.3l_0$ ,  $d = 10l_0$ , and  $\omega_1 = 5l_0$ . The result is shown in Figure 8, from which we can infer that this setup greatly affects the phase diagram as compared with Figure 2 for a uniform  $\Delta u$  surface. The transition line from  $L_{||}$  to  $L_{\perp}$  is shifted upward so that its minimum is obtained for  $L_h = l_0$  where  $\Delta u = 4.4$ . This is similar but more pronounced than the behavior seen in Figure 4 for the chemical striped surface around the  $L/l_0 = 1.0$  region.

However, when we start from a fully disordered state as initial condition inside the stable  $L_{\perp}$  region of Figure 8 (e.g.,  $L_h = 0.8l_0$  and  $\Delta u = 0.1$ ), we do not get the fully perpendicular lamellae  $L_{\perp}$  but rather a mixture of parallel and perpendicular lamellar regions (the  $L_M$  structure), as shown in Figure 9.

We find two ways to improve on the perpendicular orientation by changing the mold geometry and surface characteristics. First, we decrease the film thickness by decreasing  $L_h$  to  $0.6l_0$ . In this case, we do a gradual temperature quench, starting from the disordered state above the ODT,  $N\chi = 11.5$ , and only then proceed with a deep quench to  $N\chi = 20$ . This two-step procedure is shown in Figure 10a,b. Perfect perpendicular lamellar structures emerge. Moreover, using this two-step procedure, we can even obtain a perfect perpendicular lamellar structures with much wider  $\omega_n$  yielding  $d = 1.25 \mu\text{m}$  (or equivalently  $d/l_0 = 25$ ), as is shown in Figure 11.

A second variation is to construct the grooves from two separate materials with different A/B preference. The protruding “finger” parts are assumed to have a small A preference ( $\Delta u = u_1 > 0$ ) on both their vertical and horizontal parts, whereas the high plateau parts are taken as neutral ( $\Delta u = 0$ ).

$$\Delta u(x) = u_1 \quad \text{for } 0 \leq x \leq \omega_1$$

$$\Delta u(x) = 0 \quad \text{for } \omega_1 < x < d \quad (15)$$

With this special surface geometry and interactions, we obtain perfect  $L_{\perp}$  structures for wide range of film thicknesses. An example for such a setup with  $d = 25l_0$  periodicity is shown in Figure 12.

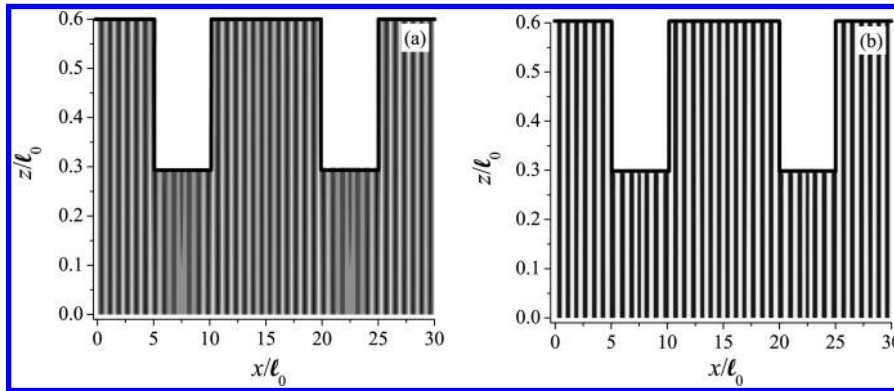
## V. Discussion and Conclusions

In this article, we addressed several surface patterns as inspired from recent experiments in relation to ordering and orientation of lamellar phases of BCP films. In the first setup, we model a BCP film confined between a chemical striped solid surface and the free film/air surface. In a second setup, the film is considered to occupy the gap between two solid surfaces; a flat one and a hard mold with specific square-shape grooves, as is inspired from recent NIL experiments.

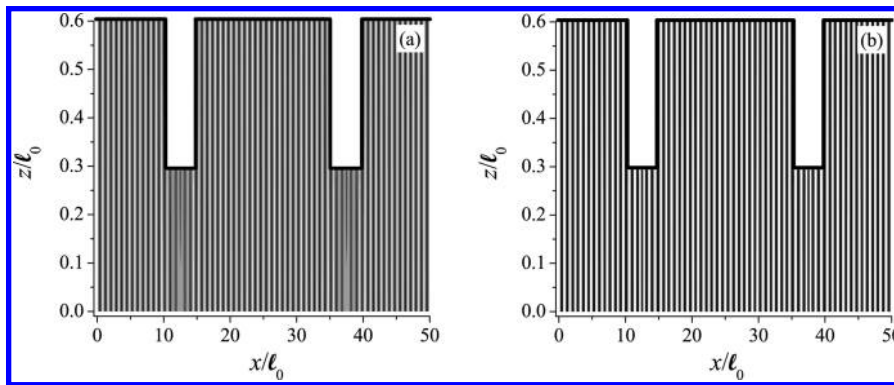
The main question that both experiments and modeling should attempt to answer is how to induce a perfect perpendicular order in BCP films. In particular, how can this be achieved by using patterned surfaces with structural features (stripes and grooves) that have a periodicity  $d$  much larger than the lamellar periodicity  $l_0$ ? Having such sparse surface features will substantially reduce the cost of large-scale production of surface templates and BCP films and is essential for applications, for example, in microelectronic and nanolithography processes.

Using the first setup of the chemical stripes on an otherwise flat and neutral surface, we are able to show that the perpendicular phase,  $L_{\perp}$ , has a larger stability region in parameter space described by the film thickness  $L$  and surface preference ( $\Delta u$ ) as compared with the homogeneous surface. Note that this is the case even for interstripe distances,  $\omega_n$ , that are one order of magnitude larger than the stripe thickness,  $\omega_s$ . This is despite the fact that the effective (averaged)  $\Delta u$  for the striped surface is smaller than the corresponding  $\Delta u$  on the homogeneous surface,  $\Delta u_{\text{eff}} = \Delta u(\omega_s/d) < \Delta u$ . We equally find that the system is very sensitive to initial conditions. Starting from a fully disordered state, above the ODT and annealing the temperature into the lamellar region, will mainly produce a mixed morphology  $L_M$ , as can be seen in Figures 5c and 6. Although the stripes nucleate growth of BCP layers on top of them (namely, domains with parallel orientation,  $L_{||}$ ), perfectly oriented perpendicular domains,  $L_{\perp}$ , are induced on top of the neutral interstripe region.

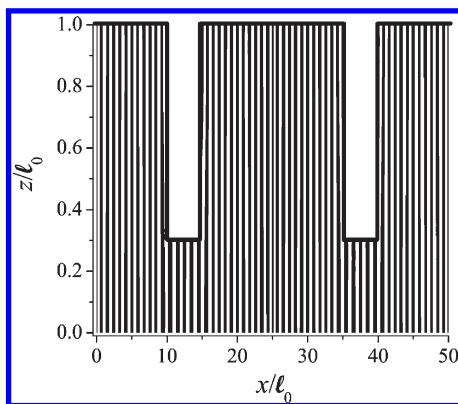
In our model, the  $L_M$  mixed morphology is a result of the large number of metastable states (local minima) that the system possesses. Although the true equilibrium is the  $L_{\perp}$  phase, it is hard to find it numerically unless one starts with the proper initial



**Figure 10.** BCP density distribution for  $d = 15l_0 = 750$  nm and  $N\chi = 11.5$  when the initial condition is the fully disordered state. The system is first annealed to (a)  $N\chi = 11.5$  and then to (b)  $N\chi = 20$ . The bottom surface ( $z = 0$ ) is neutral, and the top surface has a square grooved structure with  $\Delta u = 0.1$ . Other parameters are  $L_h = 0.6l_0$ ,  $L_l = 0.3l_0$ ,  $\omega_h = 20l_0$ , and  $\omega_l = 5l_0$ , yielding  $L = 0.5l_0$ .



**Figure 11.** BCP density distribution for wider  $d = 25l_0 = 1.25 \mu\text{m}$  using a two-step annealing procedure: first to (a)  $N\chi = 11.5$  and then to (b)  $N\chi = 20$ . The initial condition is the fully disordered state. Other parameters are:  $L_h = 0.6l_0$ ,  $L_l = 0.3l_0$ ,  $\omega_h = 20l_0$ , and  $\omega_l = 5l_0$ , yielding  $L = 0.54$ .



**Figure 12.** BCP density distribution for a heterogeneous mold with  $d = 25l_0 = 1.25 \mu\text{m}$ . The bottom surface at  $z = 0$  is neutral,  $\Delta u = 0$ . The top surface is a square grooved with  $\Delta u = 0.1$  on the sides and tips of the grooves and neutral ( $\Delta u = 0$ ) on the top plateau parts (see text and eq 15). Other parameters are  $N\chi = 20$ ,  $L_h = l_0$ ,  $L_l = 0.3l_0$ ,  $\omega_h = 20l_0$ , and  $\omega_l = 5l_0$ , yielding  $L \approx 0.86l_0$ .

conditions. This drawback should also be expected in experiments, where during sample preparation, the film undergoes many external stresses and defects are abundant. It will be of interest to verify in experiment our findings by doing a slow temperature annealing of BCP films from their disordered state (above ODT) into the lamellar region (below the ODT). Such a slow temperature annealing has the potential to produce highly oriented BCP films. Although it is not possible in all systems to reach temperatures above the ODT without damaging the BCP chains, we equally note that in many cases annealing at high

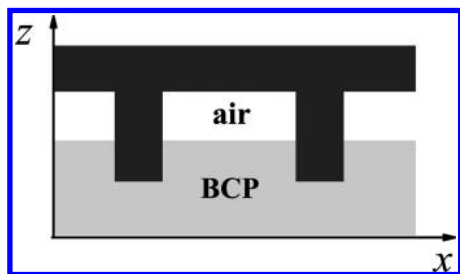
enough temperatures has the advantage that the system can reach its final state with faster kinetics.

In the second setup, we modeled a hard mold that is pressed onto a BCP lamellar film. We show that this NIL process greatly enhances perpendicular order in lamellar phases. Perfect  $L_\perp$  can be seen for film thicknesses below  $l_0$ , even when the groove width  $\omega_h$  (filled with the BCP film) is five times larger (or even larger) than the solid “finger” ( $\omega_l$ ) sections. Here the slow annealing from above ODT to below the ODT is very successful, demonstrating that this setup is more suitable for lamellar orientation purposes than the chemical stripe setups discussed above.

In Figure 12, we proposed a mold with even superior orientation qualities. For this mold, the surface preference  $\Delta u$  of the downward protrusion sections (the “fingers”) is larger than that of the top section of the groove (plateau-like). As the latter preference interferes with the  $L_\parallel$  ordering, reducing this surface preference will enhance  $L_\perp$  ordering, especially in the desired case of thin fingers and wide plateaus, where  $\omega_h \gg \omega_l$ . In experiments, it is harder to produce a mold with such specific surface characteristics as seen in Figure 12. One way would be to form it from two separate materials or to use a selective coating during mold preparation. However, creating such a mold can be a costly and delicate process that will be hard to mass reproduce.

Yet another possibility is to have an effective chemically heterogeneous mold shown in Figure 13. Suppose that the groove height is only partially filled with the BCP melt, creating pockets of air on the top of each groove.<sup>32</sup> The film/air interface within each groove can be thought of as another interface with almost neutral preference the two blocks. This situation amounts to taking different values of  $\Delta u$  on the finger-section and plateau-section of the mold. (See eq 15.) Whereas  $\Delta u = 0$  on the top section (plateau)





**Figure 13.** Schematic drawing of a NIL setup where the mold only partially is filled with the BCP film. Effectively, this means that the film sections in contact with the side boundaries of mold feel a different surface field than the top horizontal facets, which are exposed to the air.

of the groove, it is nonzero on the mold “finger” sections. This is exactly the situation explored in our calculations and shown in Figure 12, and it may be worthwhile to explore this partial filled mold in future experiments further.

Our theoretical modeling relies on numerical solutions of SCFT equations. We minimize the corresponding free energies and converge to film morphology whose free energy is an extremum using an iterative procedure. We find that the numerical procedure is sensitive to what is used as initial conditions for the BCP structure. The convergence can be toward local (metastable) states and is not always toward the true equilibrium. This is an unavoidable feature of the numerical procedure. It is not an artifact but rather reflects the true physical situation as seen in experiment. The BCP film has many metastable states separated by energy barriers, and it is hard to reach the true thermodynamical equilibrium state. Slow annealing from above the ODT or from high temperatures is one way to overcome this difficulty, at least in a partial way.

It will be of great interest to proceed further and extend our 2D calculations to full 3D calculations. This will require much longer computation times but will allow to distinguish between perfectly oriented perpendicular lamellae and those that stand up but that also wander around in the  $x$ - $y$  plane. For applications, it is important to have perfectly oriented  $L_{\perp}$  phases in the  $z$  direction that are well aligned in the lateral (in-plane) directions.

Although our present study is not exhaustive, it shows many possibilities of explaining some of the experimental findings and even points toward interesting directions for future experiments.

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